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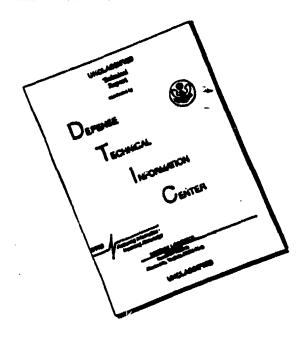
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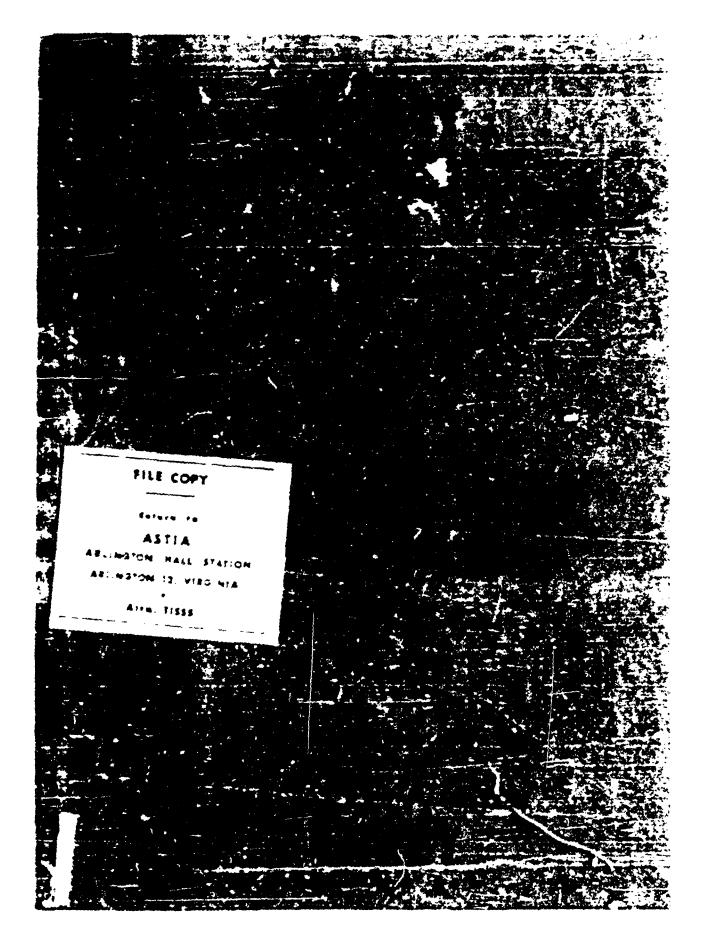
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CICARETTE PUZZ PIELD TEST (U)

Gerald V. Kinssinan

FOR THE COMMERT: Approved by:

I POUCLE

Chief, Laboratory 300



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ABSTRACT (C)

Twenty-three "Cigarette" forces were mounted in 81-ann mortar shell and tested by field firing at two increments. The score was:

16 - proper function

3 - indeterminate

2 - early

2 - no firm test

Function height varied from 1 to 6 inches above ground. These tests showed that Circurette fuzes are suitable for use with projectiles.

1. INTEODUCTION

The original Cigaretie fune was developed for a hand greenale. The entire fuze, including power supply and safety and arming mechanism, was ishricated in a package similar in size and shape to a king-cized eigerette. However, this fune was not carried beyond prototype stage. Other dome atraction models of this type of fuze had also been built (refs 2 and 3) prior to the test described in this report, but these models were not designed for firing.

The tests described herein were designed to demonstrate that Cigarette fuzes could be built to survive the conditions of projectile fixing and to function properly when approaching targets at projectile speeds.

2. CONCLUSIONS

The just showed that Cigarette fuses are suitable for une in projectiles.

3. RECOMMENDATIONS

fisveral factors should be investigated in the further development of a-c capacitance fuses. One is the possibility of eliminating neutralization of the free-space signal. Another is the effect on function height and free-space signal of the shape, position, and size of the antennas. Other forms of firing circuits should be considered, such as the use of cold-cathode thyratrons or solid-state switches.

SELECT

To increase the signar-to noise ratio and for additional protection against interserence, features such as tuned input circuit and a nehronous detection can be considered. Magnetic shielding between oscillator and amplifier may not be necessary, but additional experimental work is required to determine actual shield requirements.

4. SUMMARY OF FIRING TESTS

Twenty-three rounds were fired and the following score was obtained:

- 16 proper function
- 3 indeterminate
- 2 early
- 2 no fize test

The details of the tests are summarized in table 1.

5. Details of fixing tests

The test vehicle selected was the 31-mm mortar shell fired with two increments. The MSR fixe nose cone, the real power supply, and safety and arming mechanism were used to expect tabrication of the recessary hardware. The assembly is shown in figures 1 the real 4. Holes in the side of the shell were closed with plugs intended to blow out at detonition so that the flash would be visible.

Photographic coverage was used to obtain function by this. High-speed mouce pictures were taken at the time the shall approach—I the ...and, and low-speed pictures were taken with a background falls, marked off in feet from ground, at the spot where the shell landed. When the two pictures were sumpared, the height of the flash above the ground was obtained. The distance from nose to flash hole was subtracted to obtain the distance between the nose and the ground at the time of the flash. Actual functioning could have been somewhat him with the measured flash (about one inch) because of the motion between fram the measured flash next higher full inch. The function height varied fro. to six inches.

Firing of the 23 rounds was begun on 5 November 1958. Of two rounds fired, the first round showed a flash near the ground, and the second showed no flash. After recovery, it was determined that the second fuze had functioned. Similar troubles at a later date are discussed below.

Three more rounds were fired on 3 January 1959. The first round flashed above ground, the second had a propellent failure and did not reach arming velocity, and the third flashed above ground.

On 22 February 1959, seven rounds were fired: four were successful and three showed no flash. Fixing was then stopped until the rounds could be recovered

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TABLE 1

BOUNDS FIRED

Date	Round- Amplifier	Tetrji	Proper Proction	Peaction Beight heles	Remarks					
11-5-58	A	An Mo	Tes .		One increment One increment					
1-9-59	B)do	Yes No		Not Neutralized. Propellest failure— ince did not arm					
	В)	Yes							
2-25-59	3-B	No	36		Battery circuit was open					
	5-B 6-B	No No	Yes Yes	4 °.	Blowout plugs intact					
	7-B	No	•		Blowout plugs intact					
	8-B 10-B	No No	Tes Tes	3	Blowout plugs intact					
	11-8	No.	•	•	Three blowout plugs intact					
3-20-59	12-B	Yes	Yes	4						
	13-B 14-B	Yes	Yes Yes	6						
	20-B.	Yes	Yes	1						
	21-B	Yes	Yes	5						
	22-B	Yes	Yes	1						
	23-B	Yes	Yes	2						
	24-B	Yes	.%	_	15-sec function					
	25-B	Yes	Yes	2						
4-1-59	9-B.	Yes	Yes		I .ht to moderate rain					
	15-B	Yes	Ж		Moderate to beavy rain; 12-sec function					

[•] Indeterminate — no flash was observed but recovered fuze had functioned. Believed to be proper function but wrong orientation to see flash when no tetry! was used.

for examination. Two of the configuring remain had functioned. However, on one the plugs were intact, and on the other only one plug had been blown out. It was decided that the finals powder was not sufficiently powerful to give definite indication unless the orientation of the round happened to be suitable, and that a piece of tetryl should be substituted for one of the flash powder discs in future runds. The test vehicle had been designed and tested initially in this manner, but finals powder was substituted for the tetryl to permit recovery a successary. The third nonflashing round had the detonator in line but the detonator had not fixed. It was fixed successfully in a laboratory test. However, the 6.4-volt battery was still good days after it should have been run down and the battery connection to ground was open. Hence, the amplifler had not been energised. Therefore, this round was not considered a fixe test. A commution between a screw and a soldering lug in the potted amplifler had not been soldered, and was believed to have exceed from the shock of firing.

On 20 March 1959, nine more rounds ware fired. All functioned, but one exploded in mid-air after 15 seconds. Firing was at 30° elevation and flight time was about 24 seconds.

On April 1, 1979, two more rounds were fired. The first was fired in light to moderate rain and functioned satisfactorily. The second was fired in moderate to beary rain and functioned in mid-air after 12 seconds. The two exclusive attributed to the same unsoldered connection mentioned above. It is assumed that this connection opened from vibrate: during flight and removed the hims from the thyratron, thus causing the determition.

6. ACKNOWLEDGMENTS

John J. Furlant and James Miscampbell conducted the mechanical phases of this project. Hoyd R. Grump developed the electronic circuitry. The Model Shop fabricated the electronic equipment used in the firing tests.

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- (2) G. R. Yetter, "A Ministure Transsamorized Fuze For Mort Ranges-Cigarette Fuze," (C): DOFL Report R-51-57-19, Confidential, Jamary 1958.
- (3) Zenith Radio Corporation Final Report, Secret, DOFL Contract DA-49-186-502-CRD-578, May 1998.
- (4) Lloyd R. Crump, "A Transistor Sine Wave Oscillator," DOFL Report TR-399, June 1958. (referenced in appendix)
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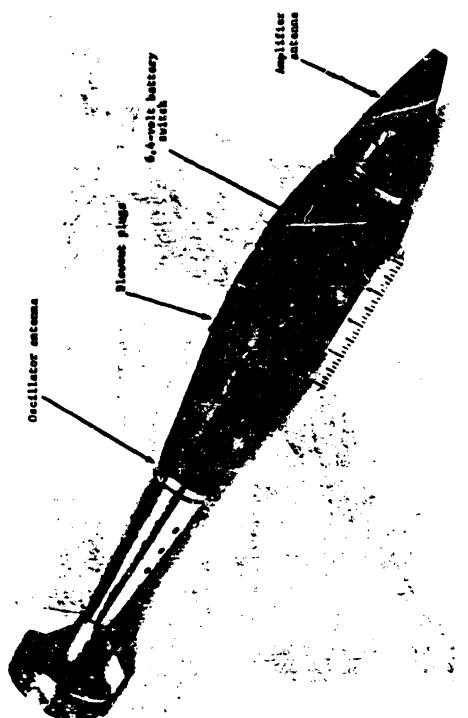


Figure 1, 61-um test vehicle-samenbled for firing,

Figure 2, 61-um test vehicle-exploded view.

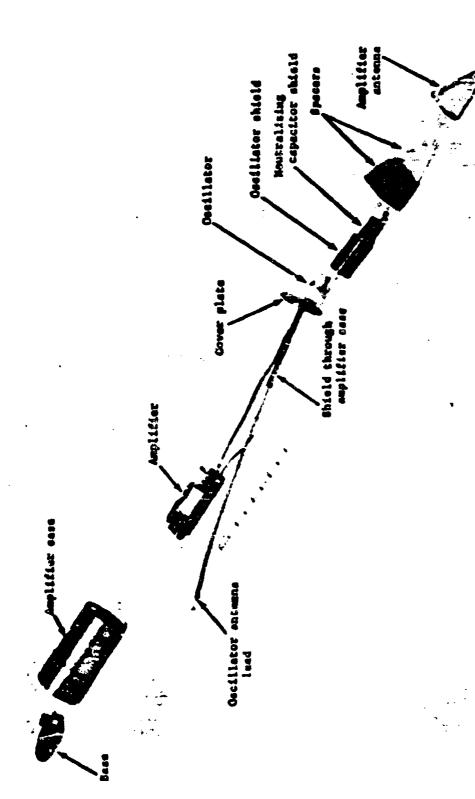


Figure 3. Amplifier and oscillator-exploded view.

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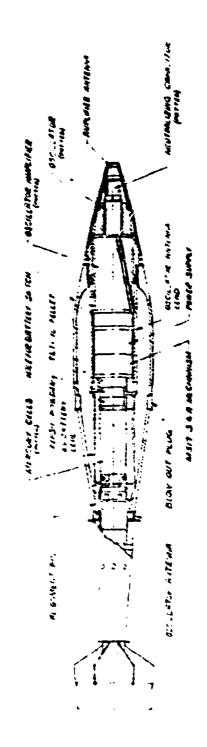


Figure 4. Bi-mm test vehicle assembly.

APPENDIX - Design Details

MECHANICAL FEATURES

Several configurations were considered for the electron. 9 packages. The arrangement used was more difficult to achieve but it was selected to simulate proposed use of the faxe. In this proposed use, the oscillator and amplifier were sulfacent to each other, and a long-shielded lead was used on the oscillator output. This arrangement required the oscillator output lead to pass through the amplifier osce. Since there was no time to determine the amount and type of shielding necessary between oscillator and amplifier, fairly heavy magnetic and electrostatic shielding was "...ed. The nose antenna of the M517 faxe was used as the amplifier antenna." In insulated ring was inserted between the shell and the tail boom for the carrantensa.

A switch for the mercury battery (in the form of a grounding screw) was added on the later models so that assembly of the package for firing could be made without having the amplifier energized. Without the switch, the round had to be fired within two hours of assembly to insure that the battery voltage had not falled off.

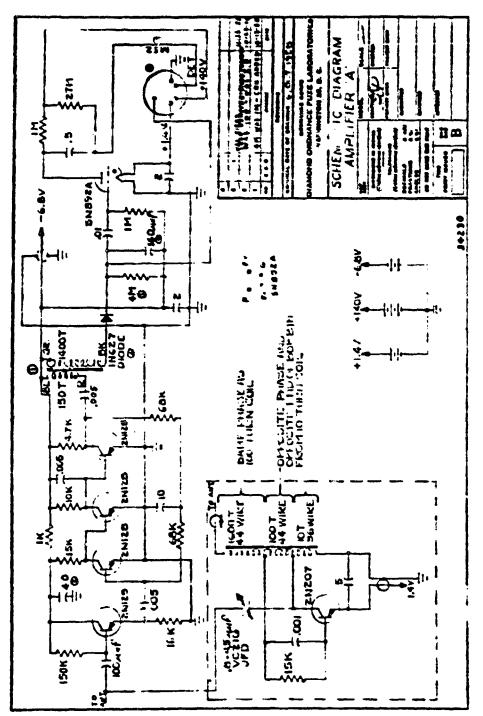
The M48 detonator was tested with an electronic breadboard simulating the proposed firing circuit of the fuze. This detonator was selected because of its short functioning time (about I microseconds). However, this detonator did not appear to be sufficiently reliable when used with the proposed circuit. (One did was obtained and, when used with a tetryl lead, the dent in the test block varied from 0.000 to 0.050 inch). These the M52 detonator, which is more sensitive and more directional in its explosive output, was tested. Its functioning time varied up to 64 microseconds when tested at 100 volts. This delay in function was considered acceptable, and the M52 detonator was selected for the field tests.

ELECTRONIC FEATURES

The oscillator was based on the circuit of reference 4. The amplifier was based on the circuit of reference 2, with output modified to use a thyratron for firing a detonator, and the bandwidth reduced for improved signal-to-noise ratio (ref 5). The firing circuit was developed to suit the application.

The oscillator was constructed in accordance with the schematic of figure 5. The first oscillator coils were wound with Ceroc wire. This wire was found to be too hard to work with because of its small size (44) and the difficulty of stripping the insulation. Wire with insulation of the Formex-Formvar-Nyclad type was substituted, and was satisfactory; sizes 36 and 42 were used. The iron core was of the shape shown in figure 6.

These oscillators had a resonant frequency of over 40 kc. When the shielded output lead was added, the frequency dropped to about 25 kc. Therefore, amplifiers were designed to peak near 25 kc. Later, with a different lot of cores the frequency of the oscillators with leads fell as low as 13 kc. The frequency was brought up to the 25 kc region by grinding the center of the core a few thousandths of an inch below the outside face, leaving a small airspace in the center leg.



Flgure 5. Schemetic diagram-amplifier A.

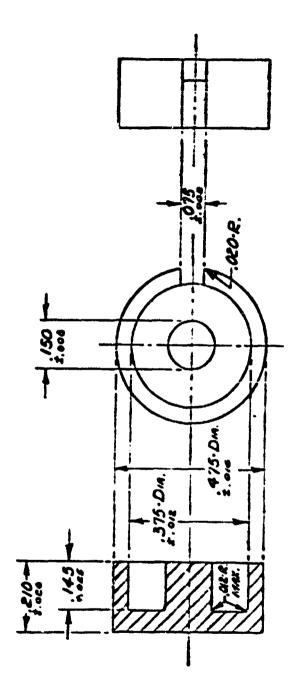


Figure 6. Pot core.

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The amplifier was also constructed in accordance with figure 5. First attempts at building the amplifier gave unsatisfactory results. Finally a working model was built by providing copper shields between the first and second stages and between the mird and fourth stages. The transformer was fabricated using the core of figure 6.

The system was checked by installing it in a shell with the intended external configuration and without the neutralizing capacitor. Oscillator and amplifier were energized with batteries contained within the shell, and a d-c voltmeter with 1-megahm resistance was inserted in the output circuit at the test lead. This voltmeter was also mounted within the shell. The shell was hung in the air with insulating cords. The "free space" signal input to the amplifier was observed to saturate the amplifier. The gain of the amplifier was lowered until the amplifier was not saturated, and then the voltage output was observed. Next, a low impedance signal source at the oscillator frequency was applied to the amplifier input. A 4-millivolt signal was required to give the amplifier output obtained in free space.

The original amplifier saturated at 15 volts de with 1.5 mv rms input. The free space signal was thus approximately three times the signal range of the amplifier. Decreasing the amplifier gain would decrease the function height. For example, if the gain were usereased so the 8-mv input would give 15 volts output, the free space output would be about 10 volts, and the function height for 15-volts output would be about 1 inch.

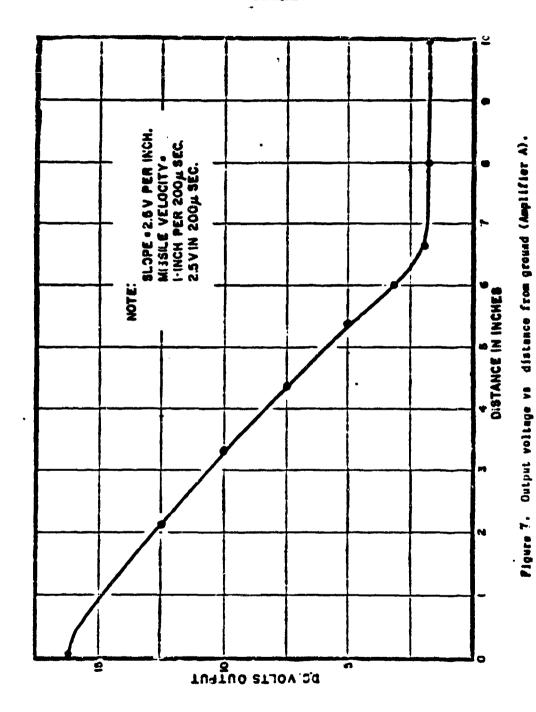
To increase the function height it was decided to retain the full amplifier gain, and to neutralize the free space signal with a 4-my signal. The phase of the 4-my signal was reversed with respect to the space signal. This neutralization was provided with a tap on the oscillator and an adjustable capacitor voltage divider to feed a signal to the amplifier antenna. With use of the adjustable capacitor the free space signal could be neutralized readily to within 0.2 my.

A shell with free space neutralization was hung on an insulating cord with mose end down, and the voltage output of the amplifier was recorded as a function of the distance from the shell to a ground plate. Typical results are shown in figure 7. The straight-line result is caused by the nonlinearity of the amplifier. A hyperbolic type of curve would result from a linear amplifier.

A differentiating network was used on the output of the amplifier so that firing of the detonator would occur on a change of signal rather than on the magnitude of the signal. The hold-off bias on the thyratron grid is -6.4 volts and the thyratron fires with a bias of about -3.0 volts. Thus a rapid 4-volt change in amplifier output is necessary to fire the round. From the curve in figure 7 it is seen that the round should fire about 4 inches above the ground. Five rounds of this type were fabricated but only two checked out suitably for firing.

At about this time it was learned that the 2N125 transistors used in the amplifier had a high failure rate when fixed at 10 increments (11,000 g. Tests were conducted with these transistors to determine if they would be suitable for use at lower accelerations. Twenty transistors were fixed in the 51-mm mortar with a charge of three increments (2000 g. Fifteen units were oriented so that the accelerating force was normal to the surface of the germanium water. Four units failed. Five units were oriented with the accelerating force parallel to the water, ad one of these failed. To reduce the Link was transistors, the two rounds refired at one increment (1000 g).

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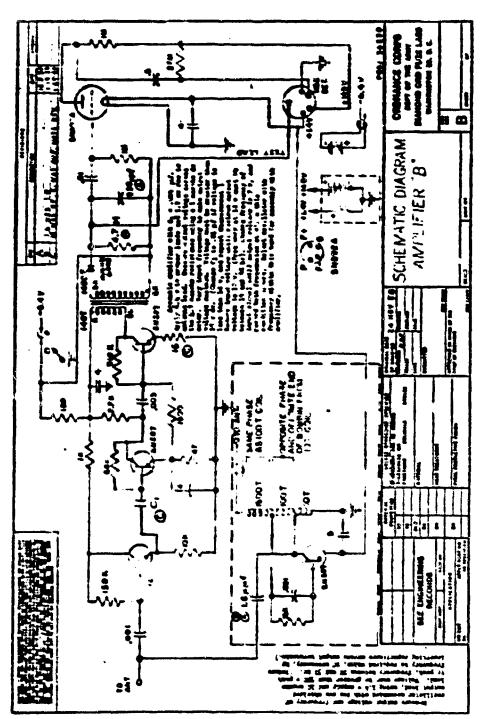
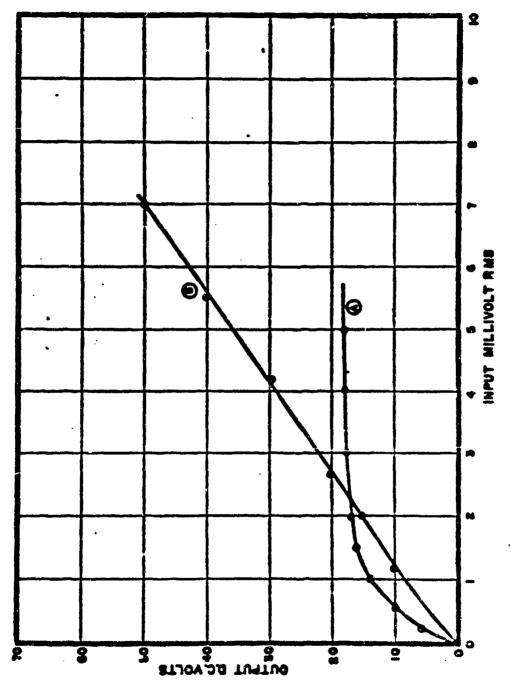


Figure 8. Schemetic diegram-amplifier B.



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Figure 9. Output veltage vs faput veltage (Amplifiers A and B).

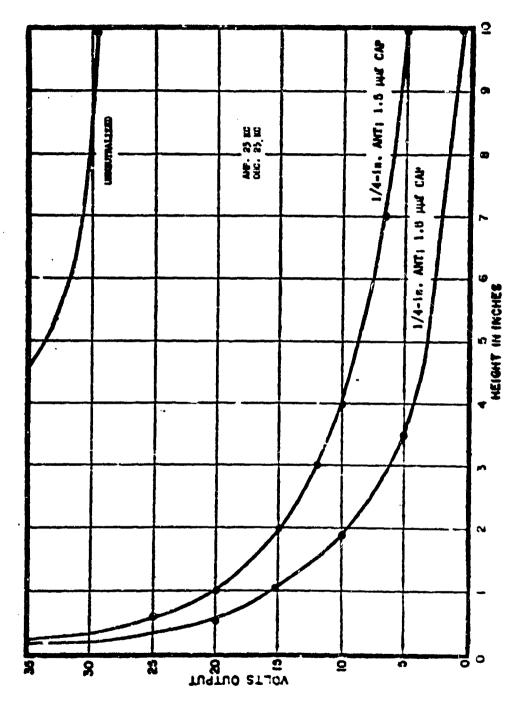


Figure 10. July to voltage vs distance from ground (Amplifler B).

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